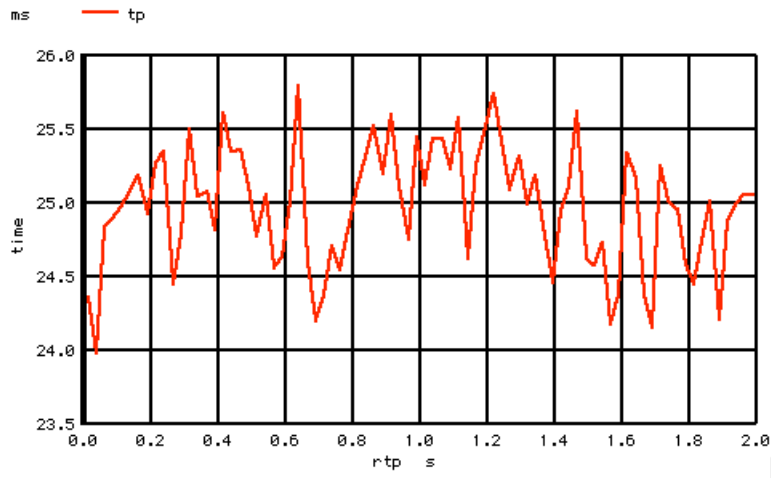


two 100mV_rms endpoints. So the ratio of the randomness to the consistent timing for C1 will be.

$$\text{randomness_tolerance} = .141/10 = 1.414\%$$

A jitter plot of the output wave form gives out about the same tolerance of the period between the edges.



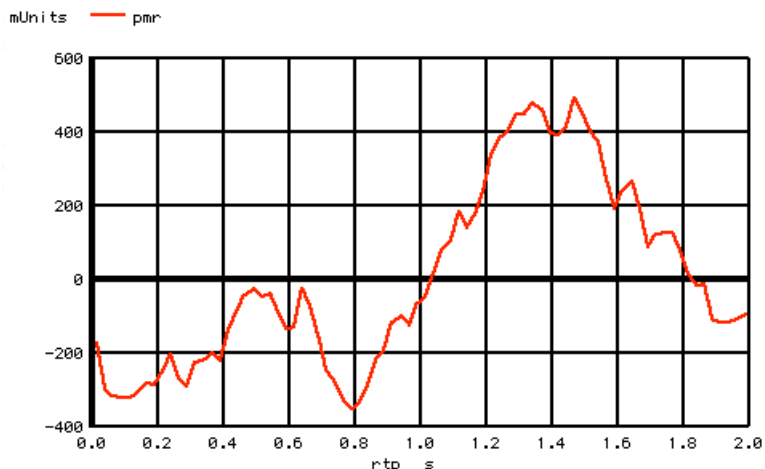
Edge2Edge_Period 0.024968 TPAC RMS SQUARE = 0.000404478

In this case **rtp** stands for **time reference point**. That is the time between when the transitions happen. The value **tp** stands for **time period**. This is the actual time between edges. Notice that the average time period is **25msec**. A 20Hz square wave has two transitions within 50msec.

The ratio of the RMS value to the Average value which was simulated is....

$$\text{TimePeriod_RMS/AVE} = 0.0162 = 1.62\%$$

But this modulation in time period is really just frequency modulation. To convert to phase modulation, one needs to integrate. The following shows the effective phase modulation in terms of radians.



Here **pmr** stands for **phase modulation radians**. When this waveform is used to phase modulate

a 20Hz square wave, it will produce almost the same spectrum as the free running oscillator which produced the jitter plot.

So how does one estimate the magnitude of the noise sidebands at 19Hz or 21Hz? There are few rules which enable this to be done.

RULE 1

Noise adds with the square root of the sum of the squares.

Capacitor C1 is seeing 100mV rms randomness at both endpoints as it toggles +/- 5 volts. That is equivalent to seeing 141mV of randomness compared to 10 volts.

RULE 2

Sampling Wide bandwidth Noise produces that same RMS magnitude regardless of the sample rate.

In this case a 100mV rms 1Khz noise signal gets sampled to a 25msec rate. The result is a 100mV rms sample signal which has a nyquist frequency of 20Hz. In other words, all the flat band noise over a 1kHz bandwidth just got aliased into a 20Hz bandwidth.

RULE 3

The total sample time period sets the resolution by which one can know frequency.

In this case the total period is 2 seconds. So the simulation has a frequency resolution of 0.5Hz.

RULE 4

Flat noise has the same amount of power in all frequency bands.

The 100mV rms noise got aliased into a 20Hz bandwidth. The fundamental frequency bin resolution is 0.5 Hz. So there are 40 frequency bins. And each bin will contain...

$$\text{Noise_per_bin} = 141\text{mV}/\sqrt{40\text{bins}} = 22.3\text{mV}_{\text{(rms)}}$$

RULE 5

Randomness in voltage maps directly to randomness in timing.

$$\text{C1_RMS_to_Ave} = 22.3\text{mV}/10 = 0.223\%_{\text{(rms)}} \text{ in time period per bin.}$$

RULE 6

FM is converted to PM by integration.

A handy rule remember when translating FM to PM could be..

When Modulating any Carrier Frequency at 1Hz
1Hz FM produces 1radian PM

Since the noise is effecting the time period, it is doing FM with white noise. If a 20Hz carrier gets modulated at 1Hz by a 1Hz FM value, it will produce a 1radian PM. Note in this case modulation is being done in magnitude format.

$$1\text{Hz}_{\text{(mag)}} \text{ FM on } 20\text{Hz} = 1/20 = 5\%_{\text{FM}_{\text{(mag)}}} \text{ \{for 1rad PM\}}$$

All frequency bins produce 0.223%_(rms) tolerance in timing. A 5%_{FM} signal at 1Hz will product 1 radian of PM. So a 0.223%_(rms) level

of FM at 1Hz will produce..

$$\text{Expected_PM} = 0.223\%/5\% = 0.0446 \text{ radians(rms) PM at 1Hz over 0.5Hz BW}$$

RULE 7

A 1 radian PM signal comes close to looking like two 50% sidebands on a spectrum. (Actually, there is some rectangular to polar conversion error.)

The output square wave is +/- 10V. It will appear as a 14.14 level at the spectrum. One radian PM will be around the 7.07 volt level. So 0.0446 radians(rms) of PM at 1Hz should have the following sideband magnitude.

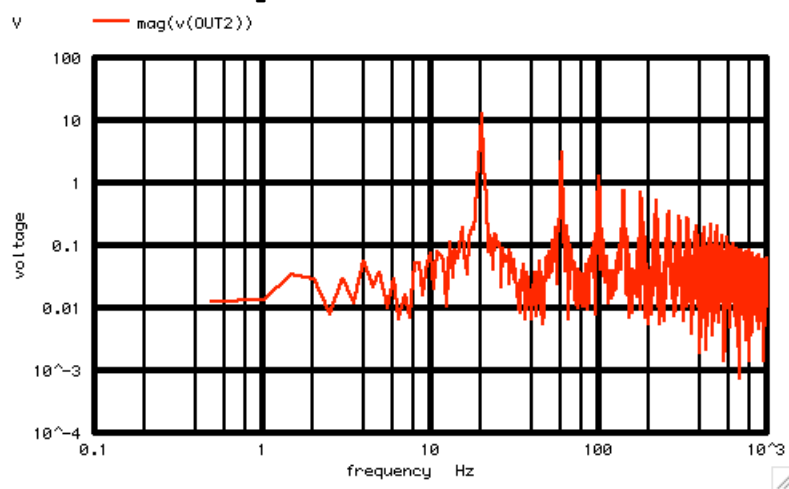
$$\text{Expect_1Hz_SideBands_rms} = 7.07 * 0.0446 = 315\text{mV_rms}$$

RULE 8

There is a 1.414 gain when converting from RMS to magnitude.

$$\text{Sideband} = 446\text{mV_ (mag)}$$

Here are the spectrum results.



But its a little hard to display the spectrum to see the +/- 1Hz side bands to any detail.

A better way might be to FFT the PM jitter file. The PWL jitter file is modeling the noise floor of a free running oscillator as simply phase modulating a 20Hz square wave by a low frequency signal.

```
FFT_the_PWL_Jitter_File
*
*   OUT  Rload
*
*   need to have a file called
*   "rndsrc" in the "MacSpice"
*   folder inside "Doucments"
*
*   First typing in a MacSpice
*   window "rndsrc .5m 1"
*
*   Then run this file
*
*   VpwlT OUT 0      PWL( + 0.0005 0.988835 +.....
* .include PWL_FileJitter.inc
Rload OUT 0 1k
*TRAN TSTEP TSTOP TSTART TMAX ?UIC?
.tran 1m 2 0 1m UIC
.control
run
set pensize = 2
plot out
```

```

let      vmag = 14.14
let      radbbgain= .5
let      gain = vmag*radbbgain
let      out2 = gain*out

```

Now a little gain scaling is needed. One would expect a 1 radian signal to appear at a level of 7.07. Macspice is already doing the rms to magnitude conversion. The data in the PWL jitter file has already been formatted into radians.

```

=====Find_Spectrum=====
linearize
set      specwindow =      "none"
*SPEC    FSTART  FSTOP    FSTEP  VECTOR
spec     .5      100     .5      v(OUT2)

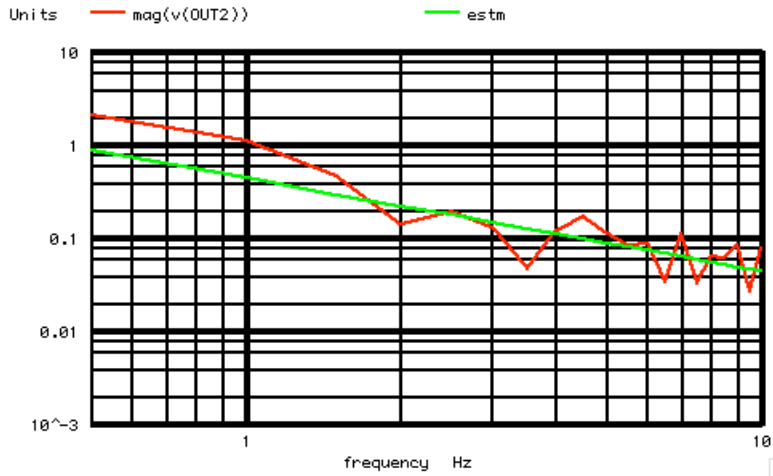
```

Why not create an estimated curve to show what the expected values would be over frequency? Use the expected **446mV** value which was calculated.

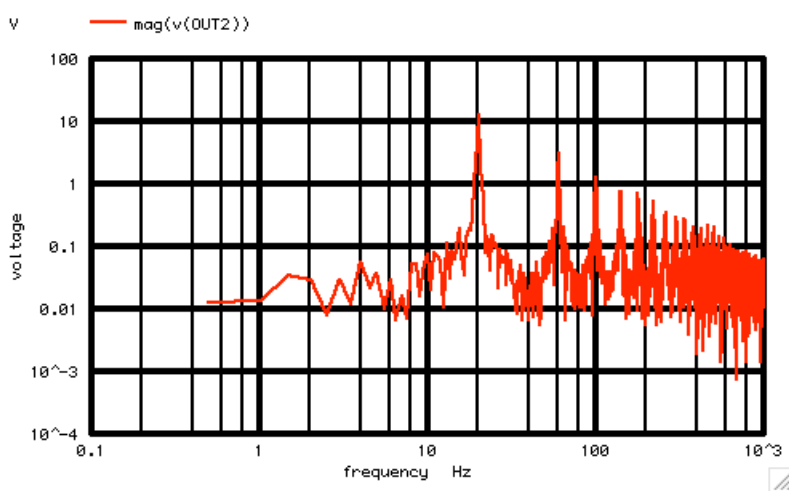
```

=====Create_Estimate_Curve=====
let      num =      length(out2)
compose  estm      start = 1 stop = $&num step =1
let      f = 1
let      i = 0
repeat  $&num
let      f = frequency[i]
let      estm[i]=.446/f
let i = i +1
endrepeat
=====Plot_Estimate_Curve=====
plot     mag(v(OUT2)) estm  loglog xlimit .5 10
.endc
.end

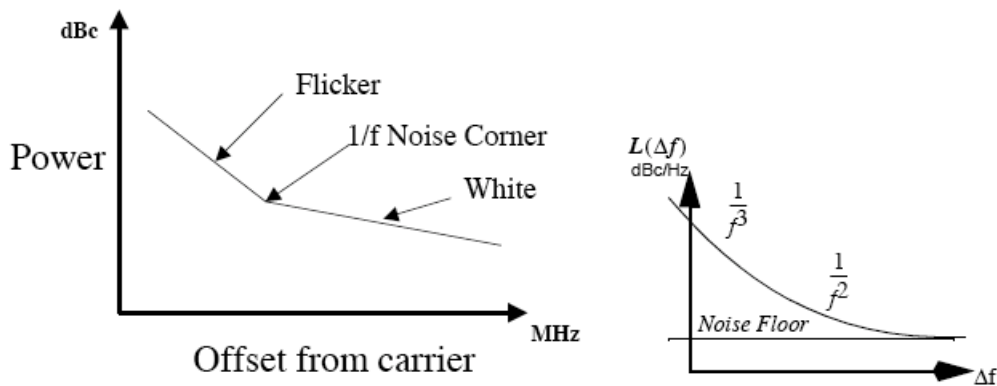
```



This is in the same scale as all the other spectrum plots. But it makes it easier to see what is happening at low frequencies



Now the effects of $1/f$ should be like modeling the low frequency noise as having some extra low frequency gain.



It is not obvious that all circuit tolerances can not be mapped to the frequency and phase domain.

```

=====Full Netlist For Copy Paste=====
FFT_the_PWL_Jitter_File
*   OUT      Rload
*
*   need to have a file called
*   "rndsrc" in the "MacSpice"
*   folder inside "Documents"
*
*   First typing in a MacSpice
*   window "rndsrc .5m 1"
*
*   Then run this file
*
*   VpwlT OUT 0      PWL( + 0.0005 0.988835 +.....
*   .include PWL_FileJitter.inc
Rload  OUT  0      1k
*TRAN  TSTEP  TSTOP  TSTART TMAX      ?UIC?
.tran  1m     2      0       1m       UIC
.control
run
set    pensize =    2
plot  out
let    vmag = 14.14
let    radbbgain= .5
let    gain = vmag*radbbgain
let    out2 = gain*out
*=====Find_Spectrum=====
linearize
set    specwindow =    "none"
*SPEC  FSTART  FSTOP   FSTEP  VECTOR
spec   .5      100    .5      v(OUT2)

```

```
*=====Create_Estimate_Curve=====
let      num =      length(out2)
compose  estm      start = 1 stop = $&num step =1
let      f = 1
let      i = 0
repeat  $&num
let      f = frequency[i]
let      estm[i]=.446/f
let i =  i +1
endrepeat
*=====Create_Estimate_Curve=====
plot      mag(v(OUT2)) estm  loglog xlimit .5 10
.endc
.end
```

2.18.10_12.15PM
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